



# Effect of Yttrium addition on magnetocaloric properties of Gd-Co-Al-Ho high entropy metallic glasses

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## ABSTRACT

The Gd<sub>25</sub>Co<sub>25</sub>Al<sub>25</sub>Ho<sub>25-x</sub>Y<sub>x</sub> (x = 1, 5, 10, and 15) high entropy metallic glasses are fabricated by copper-mold quenching technique. Substituting moderately Ho with Y effectively improves the glass-forming ability, magnetic entropy change ( $|\Delta S_M|$ ), and magnetic refrigeration capacity (RC) of Gd<sub>25</sub>Co<sub>25</sub>Al<sub>25</sub>Ho<sub>25-x</sub>Y<sub>x</sub>. Besides, the Curie temperature of this quaternary alloy can be tuned from 51 to 41 K with Y addition. Among these alloys, Gd<sub>25</sub>Co<sub>25</sub>Al<sub>25</sub>Ho<sub>20</sub>Y<sub>5</sub> exhibits the largest peak value of  $|\Delta S_M|$  up to 8.79 J kg<sup>-1</sup>K<sup>-1</sup> and the corresponding RC up to 547 J kg<sup>-1</sup> under a magnetic field of 5 T. It is worthy to note that a reverse changing trend can be observed between the maximum  $|\Delta S_M|$  and the temperature range of magnetic transition, which may be ascribed to the spatial inhomogeneity induced by yttrium microalloying. Our studies show that yttrium is an effective element to manipulate magnetocaloric properties of high entropy metallic glasses as potential refrigerants.

## 1. Introduction

Refrigeration is the process of cooling or freezing for preservative purposes by the various refrigerating machines and materials [1]. The traditional gas compression technology has been demonstrated that has many disadvantages, e.g., high energy loss, low efficiency, and environmental pollution [2,3]. Thus, the magnetic refrigeration attracts substantial attention due to its high efficiency and environmental friendliness [4,5]. The magnetic refrigeration cycle expels and absorbs heat by magnetization and demagnetization processes based on the magnetocaloric effect (MCE) that is as an inherent nature for magnetic materials [6]. Rare earth (RE) based alloys invariably exhibit excellent magnetocaloric properties due to its complex electronic structure and significant MCE [1,7,8]. It is generally accepted that RE-based magnetic refrigerants on the basis of its structure could be divided into crystalline and glassy refrigerants according to previous studies [9-11]. There are three main key parameters to evaluate the magnetocaloric properties of these refrigerants that are Curie temperature ( $T_C$ ), magnetic entropy change ( $|\Delta S_M|$ ), and temperature range of magnetic transition ( $\delta T_{FWHM}$ ) [12]. The crystalline refrigerant always possesses high magnetic transition temperature and gain MCE, e.g. Gd-Si-Ge system, thus exhibits large  $T_C$  and  $|\Delta S_M|$  [13]. However, its  $\delta T_{FWHM}$  is always very

narrow due to the first-order magnetic phase change with the structure transition [14,10], which leads to the low refrigeration capacity calculated by the product of  $|\Delta S_M|$  and  $\delta T_{FWHM}$ . As a result, the RE-based metallic glasses (MGs) have been explored due to their wide  $\delta T_{FWHM}$ . The Gd<sub>55</sub>Co<sub>20</sub>Al<sub>25</sub> bulk MG with a second-order magnetic phase change exhibits the relatively wider  $\delta T_{FWHM}$  up to 61.5 K than that of 16.4 K in the Gd<sub>5</sub>Si<sub>2</sub>Ge<sub>2</sub> alloy [15,13]. Moreover, the new alloy design concept of high entropy (HE) may extend the  $\delta T_{FWHM}$  by increasing mixed entropy that can restrain the rearrangement of magnetic moment in RE-based MG refrigerants [16].

The RE-based HE MGs are systematically investigated to further extend the  $\delta T_{FWHM}$  and obtain larger refrigeration capacity (RC) value in the past decades [8]. Among the new developed Gd<sub>25</sub>RE<sub>25</sub>Co<sub>25</sub>Al<sub>25</sub> (RE = Tb, Dy, and Ho) [17], Ho<sub>20</sub>Er<sub>20</sub>Co<sub>20</sub>Al<sub>20</sub>RE<sub>20</sub> (RE = Gd, Dy, and Tm) [18], and Gd<sub>10</sub>Tb<sub>10</sub>Dy<sub>10</sub>Ho<sub>10</sub>Er<sub>10</sub>Y<sub>10</sub>Ni<sub>10</sub>Co<sub>10</sub>Ag<sub>10</sub>Al<sub>10</sub> [19] RE-based HE MGs, the Er<sub>20</sub>Dy<sub>20</sub>Co<sub>20</sub>Al<sub>20</sub>Tm<sub>20</sub> manifests the largest  $|\Delta S_M|$  up to 11.9 J kg<sup>-1</sup>K<sup>-1</sup>, while Gd<sub>25</sub>Ho<sub>25</sub>Co<sub>25</sub>Al<sub>25</sub> possesses the largest RC up to 626 J kg<sup>-1</sup>. The outstanding magnetocaloric properties of these HE MGs may be ascribed to the high degree of the topological and chemical disorder based on the high mixing entropy in these HE MGs [17,20]. On the other hand, the HE effect also can enhance the thermal stability to improve the practicability of refrigerants during the cooling or freezing

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cycling [21,22]. Therefore, it is valuable to take efforts on developing the RE-based HE metallic refrigerants, such as  $\text{Gd}_{25}\text{Ho}_{25}\text{Co}_{25}\text{Al}_{25}$  with both large  $|\Delta S_M|$  and wide  $\delta T_{\text{FWHM}}$ . Additionally, the poor glass forming ability (GFA), high preparing cost, and settled  $T_C$  of the  $\text{Gd}_{25}\text{Ho}_{25}\text{Co}_{25}\text{Al}_{25}$  restrains its practical application as refrigerants. Substituting Ho by other cheaper elements may reduce the cost and tune  $T_C$  in a wide temperature range, and still maintains large  $|\Delta S_M|$  and RC values [23,24].

It is proposed that microalloying is an efficient method to improve the GFA, plasticity, soft magnetism, and magnetocaloric properties [25,26], which is beneficial for both crystalline and glassy refrigerants [5,24]. For example, substituting Ge with Fe of Gd-based crystalline alloy effectively reduces 90 percent of the magnetic hysteresis loss and still maintains large refrigeration capacity [5]. Besides, the adiabatic temperature change is improved by Zn addition, and  $T_C$  increases due to the substitution of Cd in Gd-based crystalline refrigerants [27]. For metallic refrigerant, the addition of Zr and Si effectively promotes the formation of  $\text{Gd}_{55}\text{Co}_{20}\text{Al}_{25-x}\text{Si}_x$  and  $\text{Gd}_{55}\text{Co}_{20}\text{Fe}_5\text{Al}_{20-x}\text{Si}_x$  ( $x = 0, 5, 10, 15$ ) HE MGs due to the small size effect and restrained nucleation rate along with HE effect [23,24,26]. Meanwhile, substituting Al by Co in Gd-Co binary MGs also improves the GFA,  $|\Delta S_M|$ , and RC [28]. For the cheaper Y element, according to the work of Lu et al., the Y addition adjusts the compositions closer to the eutectic point thereby decreases liquidus temperatures and reduces the manufacturing obstacles by means of the formation of innocuous yttrium oxides [29,30]. As reported by Nabiałek et al. [31-33], the addition of Y decreases the intensity of magnetic susceptibility disaccommodation and increases the atomic packing density, which leads to the excellent soft magnetic properties of Fe-based MGs. The partial replacement of Nb by Y in the Fe-based and Gd-based bulk MGs is useful for achieving low coercivity and outstanding soft magnetic properties as well [34,35]. Moreover, the addition of Y as the high reserves of RE element can effectively tunes  $T_C$  and improves the GFA for the  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{RE}_{25}$  MG according to our previous work [36]. It is interesting to study the microalloying effect of Y addition on the thermodynamic and magnetocaloric properties of Gd-Co-Al-Ho HE MGs to obtain the optimum composition with the largest  $|\Delta S_M|$  and GFA.

Based on the above considerations, we fabricate the  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) amorphous ribbons by melt-spinning method in this work. The influence of Y addition on GFA, thermal stability, and magnetocaloric properties are investigated in detail. The possible association between  $\delta T_{\text{FWHM}}$  and  $|\Delta S_M|$  is also discussed.

## 2. Experimental

The stoichiometric mixtures with nominal compositions of  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) were fabricated by arc melting high purity Gd, Co, Al, Ho, and Y, (above 99.9 wt.%) elements in Ti-gettered argon atmosphere. The ingots were re-melted four times to ensure the homogeneity of composition in alloys. Then small parts of ingots were cut, re-melted, and injected onto a spinning Cu roller with a linear speed of 40 m/s to prepare HE metallic ribbons. The width and thickness of the ribbons are of about 2 mm and 20  $\mu\text{m}$ , respectively. The amorphous structure of the ribbons was confirmed by X-ray diffraction (XRD) with a  $\text{Cu } K_\alpha$  radiation ( $2\theta = 10 - 80^\circ$ ) and a scanning step is 0.02°, thus the time of exposing a sample to X-ray is about 8.75 min. Thermal analysis was carried out on differential scanning calorimeter (DSC) with a heating rate of 20 K/min by using glassy ribbons. The magnetic properties of samples were measured using a superconducting quantum interference device (SQUID) magnetometer (MPMS, Quantum Design) at the temperature range between 5 and 300 K. The magnetization isotherms were measured by step of 5 K near the magnetic transition temperature under the applied field of 5 T.

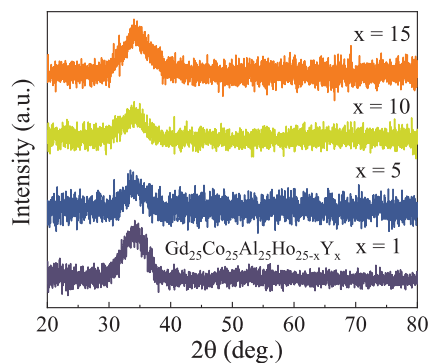


Fig. 1. XRD patterns of  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) HE metallic ribbons.

## 3. Results and discussion

Fig. 1 shows XRD patterns of the as-cast  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) ribbons. No pronounced crystalline peak appears in XRD curves and a typical broad diffraction peak is observed, indicating the amorphous nature of the glassy ribbons. The DSC traces of  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) HE metallic ribbons are presented in Fig. 2. From the DSC traces, it can be seen that an endothermic glass transition peak occurs in these samples during the heating process, followed by several exothermic crystallization peaks, demonstrating a clear glass transition.

To evaluate the GFA of  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) MGs, the GFA criteria are calculated based on the thermal parameters that are obtained from DSC profiles, such as the glass transition temperature ( $T_g$ ), the first crystalline temperature ( $T_x$ ), the melting temperature ( $T_m$ ), and the liquidus temperature ( $T_l$ ). As listed in Table 1, the reduced glass-transition temperature  $T_{rg}$  ( $T_{rg} = T_g/T_l$ ) [37], gamma parameters  $\gamma$  ( $\gamma = T_x/(T_g + T_l)$ ), and  $\gamma_m$  ( $\gamma_m = (2T_x - T_g)/T_l$ ) [38,39] show the largest values of about 0.61, 0.398, and 0.671, respectively, at the composition with  $x = 5$ . Hence, compared with the quaternary  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25}$  MG [17], substituting 5 at.% Y element effectively improves the GFA. The outstanding GFA of Y-added MGs may be attributed to large differences in atomic size between the Y and other constituent elements in this multi-component system and the large negative heating of mixing [40].

The  $T_g$ ,  $T_x$ ,  $T_m$ ,  $T_l$ , and supercooled liquid region ( $\Delta T_x = T_x - T_g$ ) at the heating rate of 20 K/min are also listed in Table 1. The temperature dependence of  $T_g$ ,  $T_x$ , and  $\Delta T$  in  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) HE MGs is drawn in Fig. 3. Evidently, the  $T_g$  increases rapidly from 625 to 633 K as the content of Y increases from 1 to 5 at.%, and reaches the largest value of 633 K at  $x = 5$ , and then decreases to 628 K with further increasing the content of Y from 10 to 15 at.%. However, the  $T_x$  almost keeps constant of 664 K. Thus, the  $\Delta T_x$  exhibits an

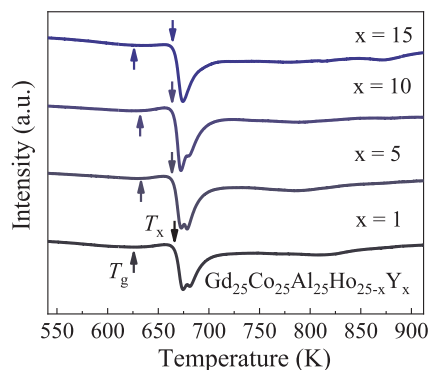
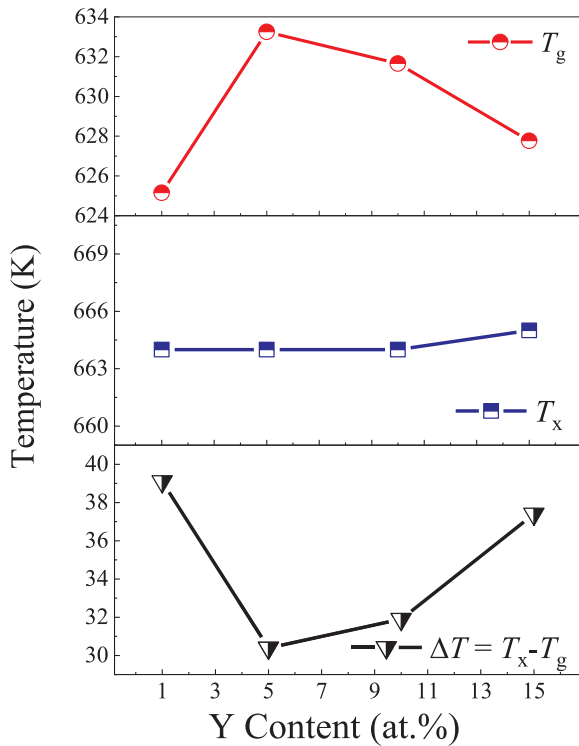


Fig. 2. DSC profiles of  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) HE metallic ribbons.

**Table 1**

The glass transition temperature  $T_g$ , first crystalline temperature  $T_x$ , supercooled liquid region  $\Delta T_x$ , melting temperature  $T_m$ , liquidus temperature  $T_l$ , reduced glass-transition temperature  $T_{rg}$ , gamma parameters  $\gamma$  and  $\gamma_m$ , and maximum magnetic entropy change  $|\Delta S_{\max}^{\text{pk}}|$  of  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) HE metallic ribbons under the external magnetic field of 5 T.

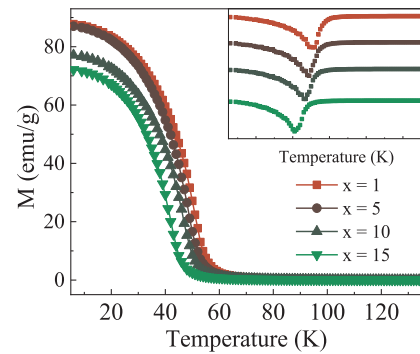
Composition	$T_g$ (K)	$T_x$ (K)	$\Delta T_x$ (K)	$T_m$ (K)	$T_l$ (K)	$T_{rg}$	$\gamma$	$\gamma_m$	$ \Delta S_{\max}^{\text{pk}} $ (J kg <sup>-1</sup> K <sup>-1</sup> )	Ref.
$\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{24}\text{Y}_1$	625.2	664	38.8	979	1058	0.59	0.395	0.665	8.63	This work
$\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{20}\text{Y}_5$	633.3	664	30.7	982	1035	0.61	0.398	0.671	8.79	This work
$\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{15}\text{Y}_{10}$	631.7	664	32.3	981	1049	0.60	0.395	0.663	7.61	This work
$\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{10}\text{Y}_{15}$	627.8	665	37.2	983	1074	0.58	0.391	0.654	7.35	This work
$\text{Gd}_{55}\text{Co}_{20}\text{Al}_{25}$	597	669	72						8.9	[23]
$\text{Gd}_{55}\text{Co}_{20}\text{Al}_{24}\text{Si}_1$	599	678	79						9.2	[23]
$\text{Gd}_{55}\text{Co}_{20}\text{Al}_{23}\text{Si}_2$	602	680	78						8.9	[23]
$\text{Gd}_{55}\text{Co}_{20}\text{Al}_{22}\text{Si}_3$	604	667	63						8.9	[23]
$\text{Gd}_{52.5}\text{Co}_{18.5}\text{Al}_{29}$	604	679	75						4.6 (2 T)	[26]
$\text{Gd}_{52.5}\text{Co}_{18.5}\text{Al}_{28}\text{Zr}_1$	604	685	81						4.7 (2 T)	[26]
$\text{Gd}_{52.5}\text{Co}_{18.5}\text{Al}_{27}\text{Zr}_2$	604	684	80						4.4 (2 T)	[26]



**Fig. 3.**  $T_g$ ,  $T_x$ , and  $\Delta T = T_x - T_g$  of  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) HE metallic ribbons as a function of Y content.

opposite changing trend as compared with  $T_g$ . For example, the  $\Delta T_x$  of  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{24}\text{Y}_1$  is 38.8 K that is similar to the quaternary  $\text{Gd}_{55}\text{Co}_{25}\text{Al}_{25}\text{Y}_{25}$  MG ( $\Delta T_x \sim 36$  K [33]). Then it reaches the minimum value of 30.7 K at the composition with 5 at.% Y, and gradually increases to 37.2 K at  $x = 15$ . It is seen that the  $\Delta T_x$  can be tuned from 30.7 to 38.8 K to improve thermal stability in a proper proportion by changing Y content in the Gd-Co-Al-Ho system. More interesting, differ from other Gd-based MG systems [23,41],  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{20}\text{Y}_5$  MGs with the most narrow supercooled liquid region exhibit the largest GFA among the studied  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  alloy system.

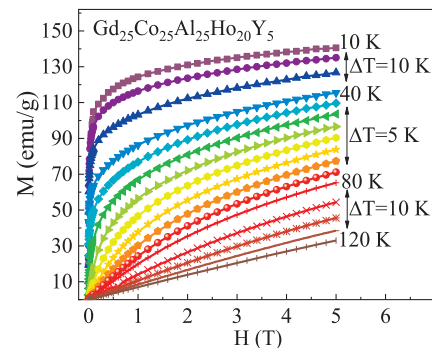
Fig. 4 presents the temperature dependence of the field cooling (FC) magnetization in  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) HE MGs under the applied magnetic field of 200 Oe. The field cooling curves were measured during the heating process after initial cooling from 300 to 5 K. Additionally, the magnetization of FC decreases and trends to zero with increasing the temperature, indicating the obvious magnetic phase transition from ferromagnetic to paramagnetic state. Meanwhile, the intensity of magnetization also decreases with the increase of Y



**Fig. 4.** Temperature dependence of the field cooling (FC) magnetization of the as-cast  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{20}\text{Y}_5$  HE metallic ribbons under the applied magnetic field of 200 Oe. The inset shows the  $dM/dT$  versus temperature curves.

content, which may be attributed to the decrease of magnetic exchange coupling in the amorphous phase [39,38]. The inset shows the  $dM/dT$  versus temperature curves. The  $T_C$  derived from  $dM/dT$  curves is 51, 49, 47, and 41 K for the composition with  $x = 1, 5, 10, \text{ and } 15$ , respectively. Obviously, the values of  $T_C$  decrease with the increase of Y content. It demonstrates that replacing partial Ho with Y element restricts the magnetic interaction and leads to a relatively stronger thermal interaction effect to exhibit the lower  $T_C$  value of MGs.

The isothermal magnetization curves of the as-cast  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{20}\text{Y}_5$  HE ribbons are plotted in Fig. 5, which can be used to evaluate the MCE measured over a wide range of temperature between 10 and 120 K. Temperature intervals of 5 K for 40 - 80 K in the vicinity of  $T_C$  and 10 K for the regions far away from  $T_C$  such as 10 - 40 K and 80 - 120 K, respectively. The magnetization of the



**Fig. 5.** The isothermal magnetization curves for the as-cast  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{20}\text{Y}_5$  HE metallic ribbons measured at the temperatures between 10 and 120 K. Temperature intervals of 5 K for 40 - 80 K and 10 K for 10 - 40 K and 80 - 120 K, respectively.

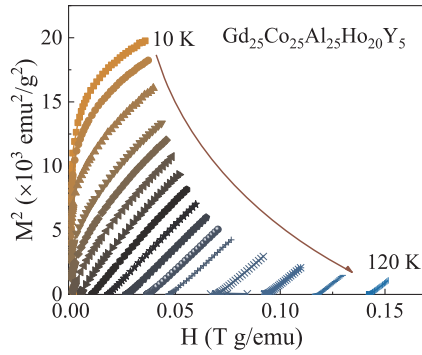


Fig. 6. The Arrott plots for  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{20}\text{Y}_5$  HE MGs measured at the temperature between the 10 and 120 K.

$\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{20}\text{Y}_5$  HE MG increases abruptly and then slowly approaches to saturation at the temperature below  $T_C$  as a result of the ferromagnetic behavior. However, the curves gradually change into straight lines with further increasing the temperature near and above  $T_C$ , indicating a transition from ferromagnetic to paramagnetic behavior.

To further identify the type of magnetic phase transition, the Arrott plots of  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{20}\text{Y}_5$  HE MG are measured at the temperature between the 10 and 120 K as one can see clearly in Fig. 6. According to the Banerjee criterion [42], the type of a magnetic phase transition can be determined by the slope of Arrott plots. The first order magnetic phase transition will display a negative slope and a positive slope is supposed to be a second order phase transition. Plots with positive slopes of  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{20}\text{Y}_5$  demonstrates a second order magnetic phase transition from ferromagnetism to paramagnetism.

The MCE of a magnetic refrigerant is mainly characterized by the  $|\Delta S_M|$ . Fig. 7 displays the  $|\Delta S_M|$  as a function of the temperature under different applied magnetic fields for the alloy with a composition of  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{20}\text{Y}_5$ , which can be calculated by integrating the Maxwell relation [15] over the applied magnetic field:

$$|\Delta S_M| = \int_{H_{\min}}^{H_{\max}} \left( \frac{\partial M}{\partial T} \right) dH \quad (1)$$

where  $H_{\min}$  and  $H_{\max}$  represent the initial and final values of the applied magnetic field, respectively. The maximal and minimal values of the magnetic field are 5 and 0 T in this work. The  $|\Delta S_M|$  increases with a larger applied magnetic field during the whole temperature range and the maximum value of  $|\Delta S_M|$  ( $|\Delta S_M^{\text{pk}}|$ ) up to  $8.79 \text{ J kg}^{-1} \text{ K}^{-1}$  for this sample. It is found that the  $|\Delta S_M^{\text{pk}}|$  also shifts to higher temperature with increasing magnetic field, which may be ascribed to the change of the magnetic free energy [17].

The  $|\Delta S_M|$  as a function of temperature in  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) HE MGs is shown in Fig. 8, which are measured under the applied field of 5 T. It is noticed that the values of  $|\Delta S_M^{\text{pk}}|$  are

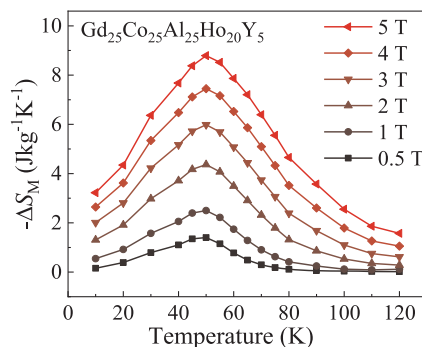


Fig. 7. Magnetic entropy changes ( $-\Delta S_M$ ) versus temperature under the applied field of 0.5, 1, 2, 3, 4, and 5 T for  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{20}\text{Y}_5$  HE MGs.

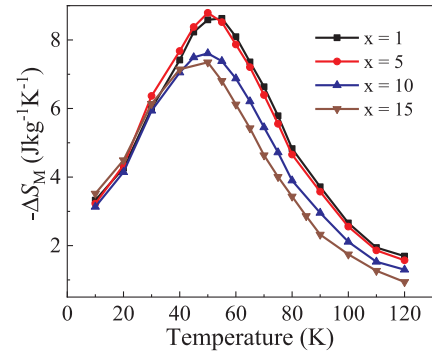


Fig. 8. Temperature dependence of magnetic entropy change ( $-\Delta S_M$ ) in  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) HE MGs under the applied field of 5 T.

8.63, 8.79, 7.61, and  $7.35 \text{ J kg}^{-1} \text{ K}^{-1}$  when  $x = 1, 5, 10, \text{ and } 15$  for  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  HE MGs under an external magnetic field of 5 T, respectively, indicating a tunable  $|\Delta S_M|$  by changing the content of Y element. On the other hands, the  $|\Delta S_M|$  curves of these samples exhibit similar peaked shape with increasing temperatures.

The refrigeration capacity (RC) is another important parameter to evaluate magnetocaloric properties by the contrast of  $|\Delta S_M|$ . The value of RC can be calculated by Gschneidner's method [43]:  $\text{RC} = |\Delta S_M^{\text{pk}}| \times \delta T_{\text{FWHM}}$ , where  $\delta T_{\text{FWHM}}$  is the full width of half maximum of  $|\Delta S_M|$ . Under an external magnetic field of 5 T, the RC values are determined to be 555, 547, 490, and  $488 \text{ J kg}^{-1}$  for the compositions with  $x = 1, 5, 10, \text{ and } 15$ , respectively. The magnetocaloric properties except for the  $|\Delta S_M^{\text{pk}}|$  for these alloys are listed in Table 2.

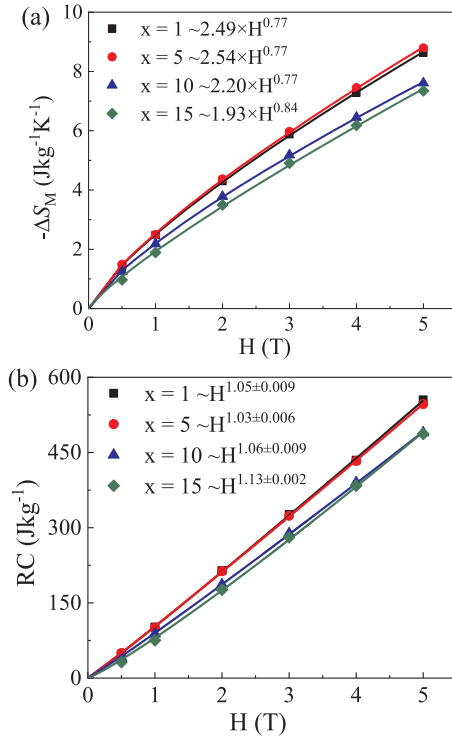
The magnetic field variation of  $|\Delta S_M^{\text{pk}}|$  and RC for the  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) HE MGs are shown in Fig. 9. One can find that the alloy of  $x = 5$  has the largest  $|\Delta S_M^{\text{pk}}|$  value under the applied field ranging from 0.5 to 5 T. The  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{24}\text{Y}_1$  exhibits the highest RC value up to  $555 \text{ J kg}^{-1}$ . Both  $|\Delta S_M^{\text{pk}}|$  and RC have a clear correlation with the applied magnetic field [44]:  $|\Delta S_M^{\text{pk}}| \propto H^n$  and  $\text{RC} \propto H^N$ . The exponents  $n$  and  $N$ , controlled by critical exponents of the alloy series, can be calculated by fitting the experimental data in Fig. 9(a-b) with the relation above. For all alloys  $x = 1, 5, \text{ and } 10$ ,  $n = 0.77$ ;  $x = 15$ ,  $n = 0.84$ . The exponents  $N$  are distinctive. For the alloy of  $x = 1$ ,  $N = 1.05 \pm 0.09$ , the alloy of  $x = 5$ ,  $N = 1.03 \pm 0.06$ ,  $x = 10$ ,  $N = 1.06 \pm 0.09$ , and the alloy of  $x = 15$ ,  $N = 1.13 \pm 0.02$ , respectively. The exponent  $n$  near the  $T_C$  is similar to that of Fe-based ( $\sim 0.75$ ), Gd-based ( $\sim 0.81$ ), and Dy-based ( $\sim 0.87$ ) MGs, which deviates from the value of  $2/3$  corresponding to mean field theory [12,16,41]. The large  $n$  value likely originates from the existence of the local inhomogeneity, e.g., chemical short-range order, or impurities [45]. As listed in Table 2, the  $n$  values increase rapidly with increasing Y from 10 to 15 at.%. It is found that the composition with a larger amount of Y, for instance more than 10 at.% Y, exhibits larger  $n$  value, which may be due to the large local inhomogeneity existed in MGs.

The  $N$  is similar to that of  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Y}_{15}\text{Dy}_{10}$  ( $\sim 1.16$ ) and  $\text{Ho}_{20}\text{Er}_{20}\text{Co}_{20}\text{Al}_{20}\text{Gd}_{20}$  ( $\sim 1.12$ ), and  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{10}\text{Y}_{15}$  ( $\sim 1.13$ ) MGs, which is slightly larger than that of  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Y}_{25}$  ( $\sim 1.01$ ) and  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Y}_{15}\text{Er}_{10}$  ( $\sim 1.03$ ) MGs [33,16]. The larger  $N$  value may be attributed to the more drastic demagnetization effect [46]. Thus, the  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{20}\text{Y}_5$  MG with the smallest  $N$  value may exhibit the lowest demagnetization effect, which leads to the strongest magnetocaloric response. This may be related to the largest value of  $|\Delta S_M^{\text{pk}}|$  in this system. Among four studied MGs, the  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{10}\text{Y}_{15}$  MG exhibits the largest  $N$  value. It implies that RC of this alloy will increase more rapidly with increasing field than that of other compositions, see Fig. 9(b). Therefore, according to the relation mentioned above, if the magnetic field is taken into consideration, the  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{10}\text{Y}_{15}$  alloy possesses more excellent magnetocaloric properties as a magnetic

**Table 2**

The magnetocaloric properties except for the maximum magnetic entropy change  $|\Delta S_{\max}^{\text{pk}}|$  and configurational entropy  $\Delta S_{\text{config}}$  for present  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) HE MGs under the external magnetic field of 5 T. The  $n$  and  $N$  are exponents of  $|\Delta S_{\max}^{\text{pk}}| \propto H^n$  and  $\text{RC} \propto H^N$ , and the  $R$  is gas constant ( $R = 8.314 \text{ Jmol}^{-1}\text{K}^{-1}$ ), respectively.

Composition	$T_C$ (K)	$\delta T_{\text{FWHM}}$ (K)	$\text{RC}$ ( $\text{J kg}^{-1}$ )	$n$	$N$	$\Delta S_{\text{config}}$
$x = 1$	51	64.31	555	$0.77 \pm 0.007$	$1.05 \pm 0.01$	1.428R
$x = 5$	49	62.17	547	$0.77 \pm 0.006$	$1.04 \pm 0.06$	1.511R
$x = 10$	47	64.32	490	$0.77 \pm 0.007$	$1.06 \pm 0.01$	1.555R
$x = 15$	41	66.32	488	$0.84 \pm 0.002$	$1.13 \pm 0.02$	1.555R

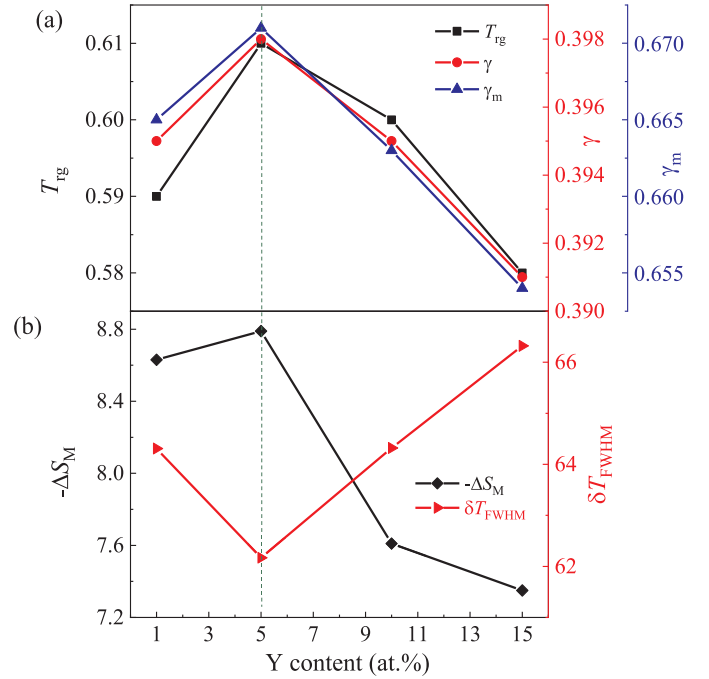


**Fig. 9.** The applied magnetic field as a function of the maximal values of magnetic entropy changes ( $-\Delta S_M$ ) (a) and RC (b) in  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) HE MGs. The solid lines are fitting curves of  $|\Delta S_M| \propto H^n$  and  $\text{RC} \propto H^N$  with standard errors.

refrigerant at a higher magnetic field as compared with others.

The changing trends of the GFA criteria and magnetocaloric parameters with the increase of substituting elements for  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) RE-based MGs are displayed in Fig. 10(a-b). From Fig. 10(a), with the addition of Y, the GFA criteria such as  $T_{\text{rg}}$ ,  $\gamma$ , and  $\gamma_m$  of  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) MGs increases from 0.59, 0.395, and 0.665 of  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{24}\text{Y}_1$  to 0.61, 0.398, and 0.671 of  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{20}\text{Y}_5$ , respectively. The further addition of Y degrades the GFA and makes  $T_{\text{rg}}$ ,  $\gamma$ , and  $\gamma_m$  decrease gradually down to much smaller values at the composition of  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{10}\text{Y}_{15}$ . Therefore, the largest values of GFA criteria ( $T_{\text{rg}}$ ,  $\gamma$ , and  $\gamma_m$ ) and  $|\Delta S_{\max}^{\text{pk}}|$  are found at the same composition of  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{20}\text{Y}_5$  (Fig. 10(a-b)), indicating the best GFA and most excellent magnetocaloric properties can be achieved in this alloy system. Additionally, the  $\Delta T$  exhibits an inverse composition dependence as compared with the  $|\Delta S_{\max}^{\text{pk}}|$  shown in Figs. 3 and 10(b). It demonstrates that the thermal parameters such as  $\Delta T$  of MGs may be related to their magnetocaloric performance. This phenomenon has not been observed in other Gd-based MGs, such as  $\text{Gd}_{55}\text{Co}_{20}\text{Al}_{25-x}\text{Si}_x$  ( $x = 0, 1, 2, \text{ and } 3$ ),  $\text{Gd}_{55}\text{Co}_{20}\text{Fe}_5\text{Al}_{20-x}\text{Si}_x$  ( $x = 0, 5, 10, 15$ ), and  $\text{Gd}_{55}\text{Co}_{20-x}\text{Al}_{24}\text{Si}_1\text{Fe}_x$  ( $x = 0, 1, 2, 3, 4, \text{ and } 5$  at.%) MGs [23,24,38]. Nevertheless, this relationship may be conducive to predict the magnetocaloric properties of similar amorphous alloy systems.

By the study of the changing-trend curves of  $|\Delta S_{\max}^{\text{pk}}|$  in



**Fig. 10.** The GFA criteria (a),  $\delta T_{\text{FWHM}}$  and  $|\Delta S_M|$  (b) as a function of Y content in  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) HE MGs.

$\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) MGs, both the Y content and the configurational entropy ( $\Delta S_{\text{config}}$ ) of magnetic elements (Gd, Co, and Ho) are the main factors that influence the magnetocaloric properties. On the basis of the previous study, we know that Y addition could affect the competition between the thermal effect and magnetic exchange interaction to tune the values of  $T_C$ . While the de Gennes factor of Y ion is zero, indicating that the Rare-Rare (R-R) exchange energy of Y element is near zero [47]. Therefore, the negligible yttrium moment results in less magnetic interactions between R-R elements, thus leading to a smaller  $|\Delta S_{\max}^{\text{pk}}|$  value with increasing Y content in present MG systems. On the other hand, the  $\Delta S_{\text{config}}$  is given by [48]  $\Delta S_{\text{config}} = -R \sum_{i=1}^n X_i \ln X_i$ , where  $n$  is the elements with configuration,  $X_i$  the mole fraction of  $i$  element, and  $R$  the gas constant:  $8.314 \text{ Jmol}^{-1}\text{K}^{-1}$ . The  $\Delta S_{\text{config}}$  of magnetic elements (Gd, Co, and Ho) are  $1.036 R$ ,  $1.015 R$ ,  $0.978 R$ , and  $0.923 R$ , respectively. Whereas, the configurational entropy  $\Delta S_{\text{config}}$  of all species of elements in the studied  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  systems are  $1.428 R$ ,  $1.511 R$ ,  $1.555 R$ , and  $1.555 R$  in  $\text{Gd}_{25}\text{Co}_{25}\text{Al}_{25}\text{Ho}_{25-x}\text{Y}_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) MGs, respectively. Following Boltzman's hypothesis on the relationship between entropy and system complexity [49], the  $\Delta S_{\text{config}}$  of magnetic elements influences the spatial inhomogeneity of MGs and bonding state between magnetic atoms, which can also influence the magnetic interactions of the studied MG systems. The spatial inhomogeneity of real ferromagnetic materials is the origin of the off-set term in the maximum  $|\Delta S_M|$  plotted against  $H^{2/3}$ , whose magnitude is proposed to be proportional to the value of  $\delta T_{\text{FWHM}}$  [50]. The composition with different  $\delta T_{\text{FWHM}}$  always leads to the variation of  $|\Delta S_{\max}^{\text{pk}}|$  in these MGs. As shown in

Fig. 10(b), the evolution of  $\delta T_{FWHM}$  as a function of Y content can be related to this fact. Therefore, the MG with lower spatial inhomogeneity and narrower  $\delta T_{FWHM}$  may exhibit a larger value of  $|\Delta S_{max}^{pk}|$ . Based on these factors, it can be concluded that the  $Gd_{25}Co_{25}Al_{25}Ho_{20}Y_5$  sample exhibiting larger  $|\Delta S_{max}^{pk}|$  than that of the compositions with less amount of Y addition like  $Gd_{25}Co_{25}Al_{25}Ho_{24}Y_1$  may be attributed to the complex spatial inhomogeneity of Y-containing MGs corresponding to the large  $\Delta S_{config}$ . On the other hand, the magnetic interactions as a dominant factor may reduce the values of  $|\Delta S_{max}^{pk}|$  when the content of Y further increases. Therefore,  $Gd_{25}Co_{25}Al_{25}Ho_{20}Y_5$  MG shows the largest value of  $|\Delta S_{max}^{pk}|$  and lowest demagnetization effect according to the smallest exponent  $N$  as shown in Fig. 9(b).

#### 4. Conclusions

In this work, the  $Gd_{25}Co_{25}Al_{25}Ho_{25-x}Y_x$  ( $x = 1, 5, 10, \text{ and } 15$ ) MGs with outstanding MCE and low cost were fabricated by copper mold casting technology. The effect of Y substitution on the improvement of thermal and magnetocaloric properties as compared with quaternary  $Gd_{25}Co_{25}Al_{25}Ho_{25}$  MGs were investigated. The results can be concluded as follows:

- (1) The addition of Y effectively improved the GFA of these alloys evaluated by the GFA criteria based on the thermal parameters. With 5 at.% Y addition,  $Gd_{25}Co_{25}Al_{25}Ho_{20}Y_5$  MG exhibits the largest criteria value such as  $T_{rg}$  of 0.61,  $\gamma$  of 0.398, and  $\gamma_m$  of 0.671, indicating the best GFA of this MG system.
- (2) The magnetization measurements showed that the  $T_C$  decreased from 51 to 41 K with the increase of Y content from 1 to 15 at.%, which may be attributed to the decrease of magnetic exchange coupling in the amorphous phase. Additionally, a non-linear relationship was displayed between the  $|\Delta S_M|$  and Y content.
- (3) Among these alloys, the  $Gd_{25}Co_{25}Al_{25}Ho_{20}Y_5$  MG exhibited the largest value of  $|\Delta S_{max}^{pk}|$  up to  $8.79 \text{ J kg}^{-1} \text{ K}^{-1}$ , the minimum value of  $\delta T_{FWHM}$  up to 62.17 K, and a relatively higher RC up to  $547 \text{ J kg}^{-1}$  under the applied field of 5 T. This result could be attributed to multiple effects of the spatial inhomogeneity and magnetic interactions between R-R elements. Such excellent MCE of Gd-Co-Al-Ho-Y HE MGs makes them attractive candidates for magnetic refrigerants.
- (4) It is particular noting that the maximal  $|\Delta S_M|$  and narrowest  $\delta T_{FWHM}$  were found in the same composition point of  $Gd_{25}Co_{25}Al_{25}Ho_{20}Y_5$ . Besides, the  $\delta T_{FWHM}$  also showed an inverse changing trend with respect to the  $|\Delta S_M|$  with increasing Y content in  $Gd_{25}Co_{25}Al_{25}Ho_{25-x}Y_x$  MGs, which may be ascribed to structural heterogeneity and the demagnetization effect corresponding to the change of critical exponent  $N$ .

#### CRedit authorship contribution statement

**C.M. Pang:** Methodology, Software, Investigation, Data curation, Visualization, Writing - original draft. **C.C. Yuan:** Conceptualization, Investigation, Writing - original draft, Writing - review & editing, Project administration, Funding acquisition, Supervision. **L. Chen:** Investigation. **H. Xu:** Investigation. **K. Guo:** Investigation. **J.C. He:** Methodology, Software. **Y. Li:** Investigation. **M.S. Wei:** Methodology. **X.M. Wang:** Methodology, Writing - review & editing. **J.T. Huo:** Writing - review & editing. **B.L. Shen:** Writing - review & editing, Project administration, Funding acquisition.

#### Declaration of Competing Interest

None.

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